

## Preparation and Characterization of K<sub>2</sub>CO<sub>3</sub>-Activated Kraft Lignin Carbon

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A series of activated carbons (ACs) were prepared by K<sub>2</sub>CO<sub>3</sub> activation from kraft lignin (KL) that was recovered from papermaking black liquor. The effects of process parameters such as the activation temperature (AT), activated period, K<sub>2</sub>CO<sub>3</sub> to KL mass ratio, and N<sub>2</sub> flow rate on the characteristics of the final product were determined. The ACs were characterized using nitrogen adsorption, morphology, and fractal dimension analyses. The results showed that the AT was the main factor influencing the yield, surface area, and pore structure. The yield of ACs obviously decreased from 50.6% to 20.5% with increasing AT from 600 °C to 1000 °C, and decreased with increasing K<sub>2</sub>CO<sub>3</sub>/KL mass ratio. Activation time and N<sub>2</sub> flow rate had slight effect on the yield of ACs. The surface area and total pore volume increased as the AT rose to 900 °C and then decreased with further increases in temperature. The maximum surface area and total pore volume were 1816.3 m<sup>2</sup>/g and 1.26 cm<sup>3</sup>/g, respectively, at a K<sub>2</sub>CO<sub>3</sub> to KL mass ratio of 3:1, AT of 900 °C, activation time of 2 h, and N<sub>2</sub> flow rate of 70 cm<sup>3</sup>/min. The pore structure of the ACs could be tailored by controlling the AT. As the AT was increased from 700 to 1000 °C, the mesoporosity increased from 11.6% to 95.9%. SEM images indicated that the morphology of ACs was modified by the AT. The K<sub>2</sub>CO<sub>3</sub> was partially recycled.

*Keywords:* Kraft lignin; K<sub>2</sub>CO<sub>3</sub>; Chemical activation; Activated carbon; Structural characterization

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### INTRODUCTION

Activated carbon (AC) is the most popularly used absorbent for gas- and liquid-phase applications, and also for capacitor and catalyst support products (Zhang *et al.* 2014a; Li *et al.* 2015). Due to its low cost and renewability, the biomass from industrial wastes, agricultural, or forestry by-products, as a precursor for AC production, has received much attention (Liu *et al.* 2015; Jain *et al.* 2016). Lignin is the second most abundant natural polymer and most abundant phenolic polymer with substituted phenylpropane units, that represents a major component of non-edible biomass (Bu *et al.* 2012). Lignin contributes as much as 30% of the weight and as much as 40% of the energy content of lignocellulosic biomass (Lange *et al.* 2013). Kraft lignin (KL) is a byproduct of biomass pulping; most KL is now directly burned to generate energy, which is a disadvantage because the storage of fuel is often complicated and oftentimes requires immediate use. Moreover, the emission of flammable gas and ash could result in environmental problems (Kang *et al.* 2013). Because KL has a high carbon content, it is a suitable precursor for the preparation of activated carbon (Suhast *et al.* 2007).

A few studies used chemical activation with KOH, NaOH,  $K_2CO_3$ ,  $Na_2CO_3$ ,  $H_3PO_4$  or  $ZnCl_2$ , and physical activation with  $CO_2$  or steam to prepare KL-ACs (Carrott *et al.* 2008; Torné-Fernández *et al.* 2009; Huang *et al.* 2014; Saha *et al.* 2014). Among the alkaline chemical activating agents, KOH and  $K_2CO_3$  are preferred (Babel and Jurewicz 2008; Xia *et al.* 2015). Hayashi *et al.* (2000) examined the influence of the activating reagents  $K_2CO_3$  and KOH on the pore structure of KL-ACs. The results indicated that the surface area and pore volume of  $K_2CO_3$  activated AC exceeded that of carbon activated with KOH at the same activation temperature. Moreover, both ACs were mainly microporous carbon. Foo *et al.* (2011) used rice husks as a feedstock for preparation of activated carbon by microwave induced KOH and  $K_2CO_3$  activation. Their results revealed that the  $K_2CO_3$ -activated sample showed higher yield and better pore structures and adsorption capacity development than the KOH-activated sample. These studies focused on the characteristics of the final product such as the surface area, pore volume and pore size distribution. However, very few studies have involved the tailored mesopore AC preparation, fractal dimension characterization of AC, and activating agent recovery (Song *et al.* 2012; Li *et al.* 2014). Moreover, KOH as an activating agent has some disadvantages, such as a strong erosion rate, high cost, and low carbon yield. Compared with KOH,  $K_2CO_3$  is less expensive and capable of green recycling (Liu *et al.* 2012).

In the present work, KL-activated carbons were prepared using a simple, one-step  $K_2CO_3$  activation method, as shown in Fig. 1. After activation, a portion of  $K_2CO_3$  was recovered from the washing water by crystallization, and some of the washing water was reused as primary washing water so that the emission of alkaline washing wastewater could be reduced. The influence of the activation temperature, mass ratio of  $K_2CO_3$  to Kraft lignin, activation time, flow rate of  $N_2$  gas on the carbon yield, specific surface area, and pore structure of the activated carbons was investigated.

## EXPERIMENTAL

### Materials and Reagents

Industrial-grade KL was purchased from the Xuemei Paper Mill in Shandong Province (Shandong, China) and was used for an acid de-ash pretreatment. Analytical-grade  $H_2SO_4$  (98%) and  $K_2CO_3$  were purchased from the Sinopharm Chemical Reagent Co. (Chengdu, China). High-purity  $N_2$  was obtained from the Mianyang Special Gases Factory (Minyang, China).

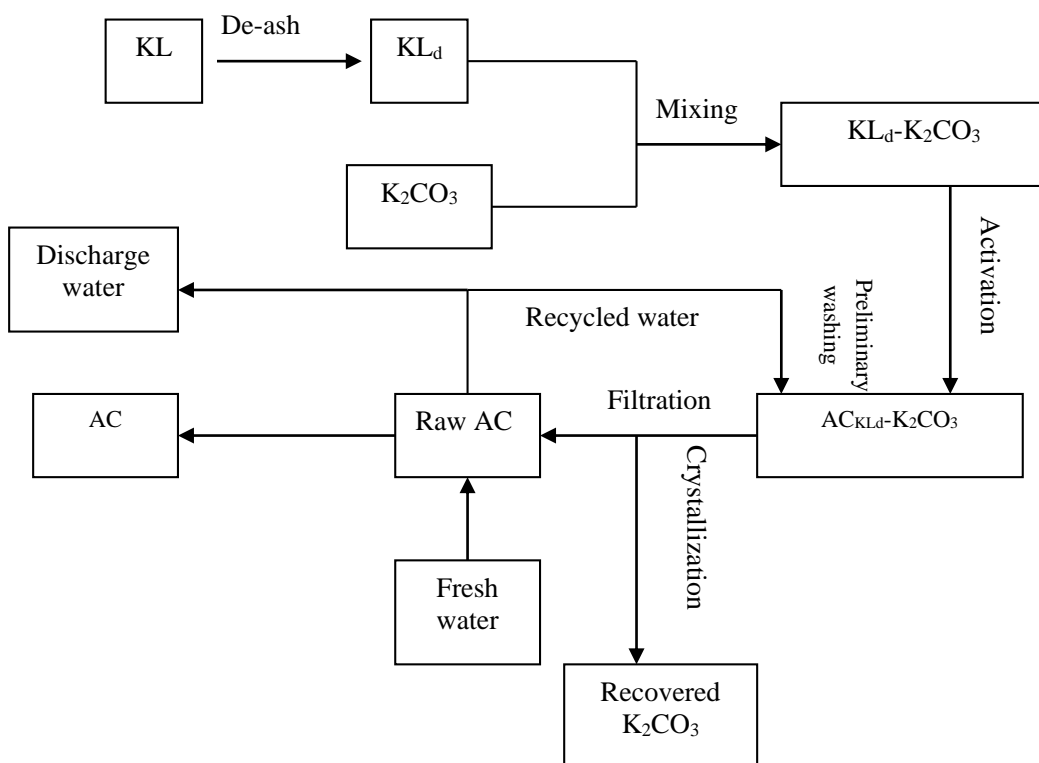
### Preparation of the ACs

The acid de-ash pretreatment process of KL, based on previous literature (Fierro *et al.* 2007), was used to prepare the deash KL ( $KL_d$ ). The activation process of  $KL_d$  is shown in Fig. 1. During the activation procedure, 5.0 g of  $KL_d$  was physically mixed with powdery  $K_2CO_3$  using various  $K_2CO_3$  to  $KL_d$  mass ratio of 1:1, 2:1, 3:1, and 4:1. The mixed sample was set on a ceramic boat that was then inserted into a stainless steel reaction tube (diameter of 50 mm). The carbonization and activation of  $KL_d$  were carried out in a horizontal tube furnace flushed with nitrogen. The activation conditions are as follows: heating rate of 10 °C/min, activation temperature of 600 to 1000 °C, activation time of 1 to 3 h, and  $N_2$  flow rate of 40 to 100  $cm^3/min$ . At the end of activation, the samples were cooled down under same  $N_2$  flow rate. The activated samples were preliminarily washed repeatedly with 50 mL of circulating water for three times and separated according to solid and filtrate portions.

The three incorporative filtrate was concentrated by rotation distillation and crystallized to recover the  $K_2CO_3$ . The solid portion was washed with distilled water until it had been neutralized. The washed samples were dried at 105 °C for 12 h and then ground to form the activated carbon powder.

### ACs Characterization

The surface area, pore volume, and pore diameter were determined from the corresponding nitrogen adsorption-desorption isotherms obtained at 77 K with an automatic instrument (TriStar II 3020 V1.03, Micromeritics, Norcross, GA, USA). Prior to the adsorption measurements, all samples were outgassed in a vacuum at 300 °C for 300 min. The specific surface area was calculated using the Brunauer-Emmett-Teller (BET) method, and the total pore volume was calculated using the adsorption data at a relative pressure of 0.973. The micropore area and volume and the mesopore surface area were obtained from the t-plot method. The average pore diameter was calculated from the  $N_2$  adsorption isotherm using the Barrett-Joyner-Halenda (BJH) method.



**Fig. 1.** Schematic of the preparation of ACs from  $KL_d$  by  $K_2CO_3$  activation

The surface morphologies of the ACs were imaged using a scanning electron microscope (SEM) (Model JSM-6700F, JEOL Ltd., Tokyo, Japan).

The recovery ratio of  $K_2CO_3$  was calculated using Eq. 1,

$$Recovery\% = \frac{m_1 - m_{AC}}{m_2} \times 100\% \quad (1)$$

where *Recovery%* is recovery ratio of  $K_2CO_3$ ,  $m_1$  is the mass of  $AC_{KLd}-K_2CO_3$  mixture after activation and before washing,  $m_{AC}$  is the final AC mass, and  $m_2$  is the initial  $K_2CO_3$  mass.

The fractal dimension, which is a measurement of roughness or irregularity, was determined by applying the following Frenkel-Halsey-Hill (FHH) equation (Hayashi *et al.* 2002) to the N<sub>2</sub> adsorption isotherm on ACs at 77 K.

$$V = K \left[ \ln \left( \frac{P_0}{P} \right) \right]^{D-3} \quad (2)$$

where  $V$  is the liquid nitrogen amount adsorbed by filling micropore volume at a relative pressure ( $P/P_0$ ) between 0.0 and 0.3,  $P_0$  is saturation pressure,  $P$  is adsorption pressure,  $K$  is a constant, and  $D$  is the fractal dimension. The logarithm of the amount adsorbed ( $V$ ) and the logarithm of  $\ln(P_0/P)$  are shown in the FHH plot. The linear behavior and the fractal dimension ( $D$ ) make up the slope.

## RESULTS AND DISCUSSION

The effect of the activation temperature on the carbon yield is shown in Table 1 (entries 1 to 5). The results revealed that the yield decreased from 50.6% to 20.5% when the activation temperature was increased from 600 to 1000 °C. A higher activation temperature released more volatiles and therefore reduced the carbon yield.

**Table 1.** Textural Characteristics of ACs Obtained by K<sub>2</sub>CO<sub>3</sub> Activation

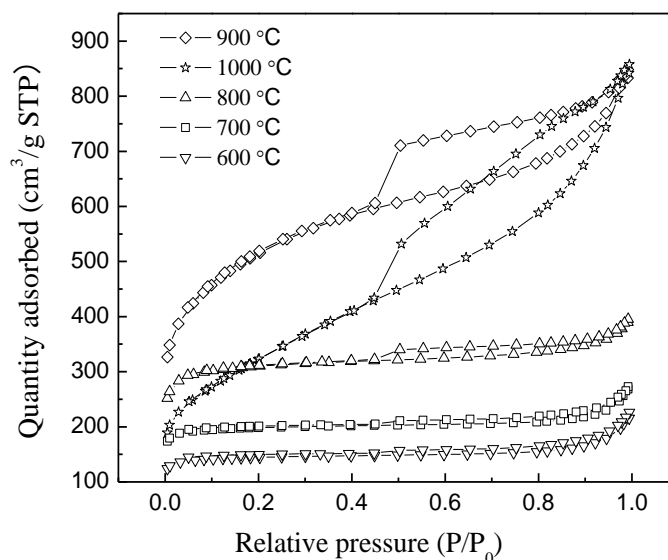
Entry	AC <sub>R-T-t-v</sub> <sup>1</sup>	A <sub>BET</sub> <sup>2</sup> (m <sup>2</sup> /g)	A <sub>e</sub> <sup>3</sup> (m <sup>2</sup> /g)	Mesopore proportion (%)	V <sub>t</sub> <sup>4</sup> (cm <sup>3</sup> /g)	V <sub>micro</sub> <sup>5</sup> (cm <sup>3</sup> /g)	D <sup>6</sup> (nm)	Y <sup>7</sup> (%)
1	AC <sub>3-600-2-70</sub>	483.6	65.0	13.4	0.31	0.20	2.5	50.6
2	AC <sub>3-700-2-70</sub>	666.4	77.2	11.6	0.38	0.27	2.3	49.5
3	AC <sub>3-800-2-70</sub>	1041.4	179.5	17.2	0.57	0.40	2.2	47.4
4	AC <sub>3-900-2-70</sub>	1816.3	1229.9	67.7	1.26	0.26	2.8	35.6
5	AC <sub>3-1000-2-70</sub>	1166.5	1118.6	95.9	1.23	0.01	4.2	20.5
6	AC <sub>1-900-2-70</sub>	1481.6	432.3	29.2	0.86	0.48	2.3	43.1
7	AC <sub>2-900-2-70</sub>	1564.6	573.1	36.6	0.95	0.46	2.4	38.6
8	AC <sub>4-900-2-70</sub>	1567.8	506.2	32.2	0.98	0.49	2.5	32.3
9	AC <sub>3-900-1-70</sub>	1458.1	346.3	23.8	0.83	0.52	2.3	36.9
10	AC <sub>3-900-3-70</sub>	1586.8	497.0	31.3	0.94	0.50	2.4	33.5
11	AC <sub>3-900-2-40</sub>	1402.6	396.8	28.3	0.81	0.47	2.3	32.7
12	AC <sub>3-900-2-100</sub>	1528.6	517.5	33.6	0.89	0.47	2.3	38.2

1 AC: activated carbon; R: K<sub>2</sub>CO<sub>3</sub> to KL<sub>d</sub> ratio; T: activation temperature (°C); t: dwell time (h); and v: N<sub>2</sub> flow rate (cm<sup>3</sup>/min); 2 A<sub>BET</sub>: BET surface area of AC; 3 A<sub>e</sub>: external surface area of AC; 4 V<sub>t</sub>: total pore volume of AC; 5 V<sub>micro</sub>: micropore volume of AC; 6 D: average pore diameter of AC; 7 Y: yield of AC.

The effects of the activation temperature on the surface area and the pore volume are also shown in Table 1 (entries 1 to 5). As the activation temperature was increased from 600 to 900 °C, the surface area increased from 483.6 to 1816.3 m<sup>2</sup>/g. However, further increases in the activation temperature (from 900 to 1000 °C) led to a marked decrease in carbon surface area, from 1816.3 to 1166.5 m<sup>2</sup>/g due to the micropores having been widened or (and) merged to mesopores and macropores. In addition, at low activation temperatures, such as 600 °C, the main pore structure of the AC is microporous. However, as the activation temperature was increased to 1000 °C, the proportion of mesopores increased up to 95.9%. This increase in the mesopore volume fraction at 1000 °C may be

a result of some micropores creating larger pores (merged or widened of micropores). When the activation temperature was increased from 600 to 1000 °C, the average pore diameter increased from 2.5 to 4.2 nm.

Figure 2 shows the nitrogen adsorption-desorption isotherms of ACs prepared at various temperatures. The N<sub>2</sub> uptake increased with the increase in activation temperature and reached a maximum at 900 °C. Increasing the activation temperature to 1000 °C resulted in a partial decrease in the N<sub>2</sub> uptake.



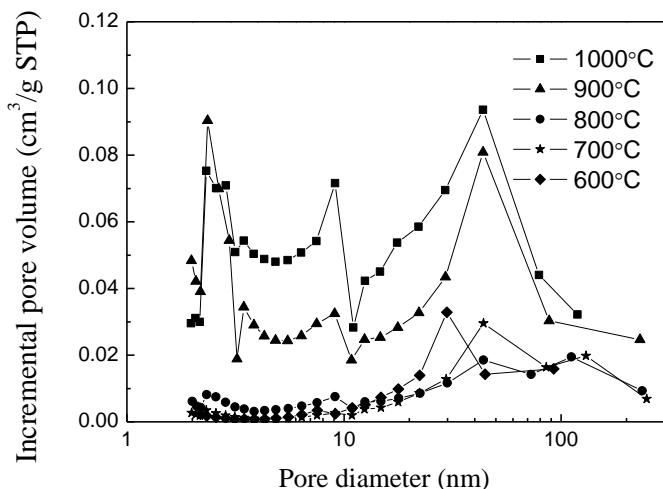
**Fig. 2.** Nitrogen adsorption isotherms of ACs obtained by K<sub>2</sub>CO<sub>3</sub> at various activation temperatures (R = 3; t = 2 h; v = 70 cm<sup>3</sup>/min)

In Fig. 2 no obvious hysteresis can be observed in the range 600 to 700 °C, indicating that the isotherms belonged to a type I of the IUPAC classification, characteristic of microporous materials. However, the isotherms at 900 and 1000 °C exhibited apparent hysteresis loops. This adsorption behavior is classified as a type IV isotherm, which implies that the ACs were highly mesoporous. This result indicates that the pore structure of the ACs could be tailored by controlling the activation temperature.

Figure 3 shows the pore size distributions of the ACs prepared from KL<sub>d</sub> with different AT. ACs obtained at 600 to 800 °C suggested predominant micropores due to only slight incremental increases in mesoporous and macroporous volume. However, the ACs activated at 900 and 1000 °C have more mesopores and macroporous due to more incremental mesoporous and macroporous volume. This was in accordance with the results from the adsorption isotherms, as shown in Fig. 2.

The effect of the K<sub>2</sub>CO<sub>3</sub>/KL<sub>d</sub> mass ratios on the carbon yield, BET surface area, and pore volumes is also shown in Table 1 (entries 4, 6, 7, and 8). The carbon yield decreased with increases in the K<sub>2</sub>CO<sub>3</sub>/KL<sub>d</sub> mass ratio. This may be due to the higher the mass ratio of K<sub>2</sub>CO<sub>3</sub>/KL<sub>d</sub> (the mass of KL<sub>d</sub> is constant), the more K<sub>2</sub>CO<sub>3</sub> reacted with carbon, and the more carbon was consumed, so that the yield of activated carbon decreased.

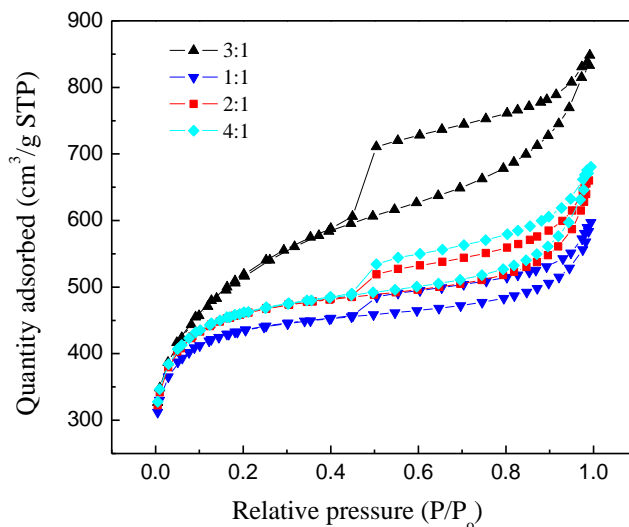




**Fig. 3.** Pore size distribution of ACs activated at various AT

As the mass ratios increased from 1 to 3, the BET surface area and pore volume also increased. This occurred because of an increase in the contact area between  $KL_d$  and the activating agent. This in turn increased the release of volatiles and the pore surface area. However, further increases in the mass ratio from 3 to 4 resulted in a decrease in the BET surface area and pore volume. This may be due to the higher  $K_2CO_3/KL_d$  mass ratio produce an extensive breaking of network structure of  $KL_d$  by alkali reagent, the shrinkage of the structure and consequently the reduction of the surface area and the total pore volume.

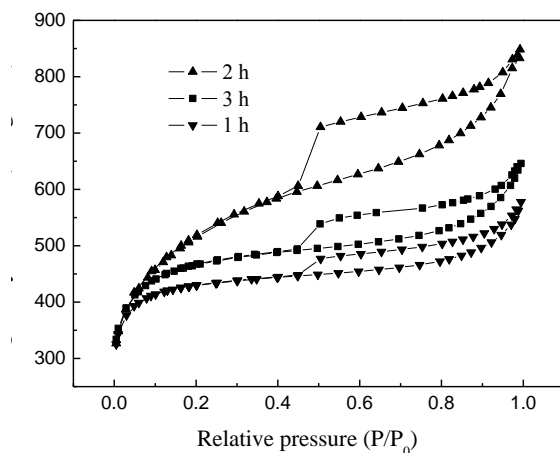
Figure 4 depicts the  $N_2$  adsorption-desorption isotherms of ACs at various  $K_2CO_3/KL_d$  mass ratios. All isotherms displayed an abrupt increase in the adsorbed volume at a low relative pressure ( $P/P_0$ ), indicating the presence of a large proportion of micropores. Furthermore, as the relative pressure increased to 0.4, the isotherms exhibited apparent hysteresis loops. This adsorption behavior exhibited a type IV isotherm, characteristic of mesoporous structure. Therefore, the ACs obtained at different  $K_2CO_3/KL_d$  mass ratios were both microporous and mesoporous in structure.



**Fig. 4.** Nitrogen adsorption isotherms of ACs obtained by a one-step activation method from various mass ratios of  $K_2CO_3$  to  $KL_d$  (AT = 900 °C; t = 2 h; v = 70  $cm^3/min$ )

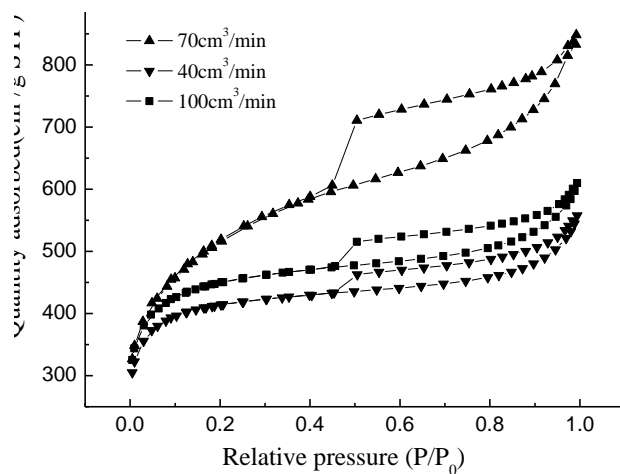
The effects of the activation period on the carbon yield, BET surface area, and pore volumes are also shown in Table 1 (entries 4, 9, and 10). The carbon yield decreased slightly when the activation period was extended; this was primarily because of the promotion of carbon burn off and tar volatilization caused by a longer holding time. Both the  $S_{\text{BET}}$  and pore volumes of the resultant ACs increased slightly with increasing activation period up to 2 h. When the activation period was above 2 h, the  $S_{\text{BET}}$  decreased slightly from 1816.3 to 1586.8  $\text{m}^2/\text{g}$ . This was because the excessive activation time led to the collapse of the pores; therefore, the surface area and pore volume became smaller. The results show that the 2-h activation period was a suitable length of time for carbon activation.

Figure 5 shows the pore characteristics of samples activated with  $\text{K}_2\text{CO}_3$  at various activation periods. All isotherms exhibit a type IV isotherm with a pronounced desorption hysteresis loop, which is evidence of the presence of mesopores. Moreover, adsorption occurs at relatively low pressure, indicating the existence of micropores. These results indicate that the pore structure of ACs at various periods was both microporous and mesoporous.

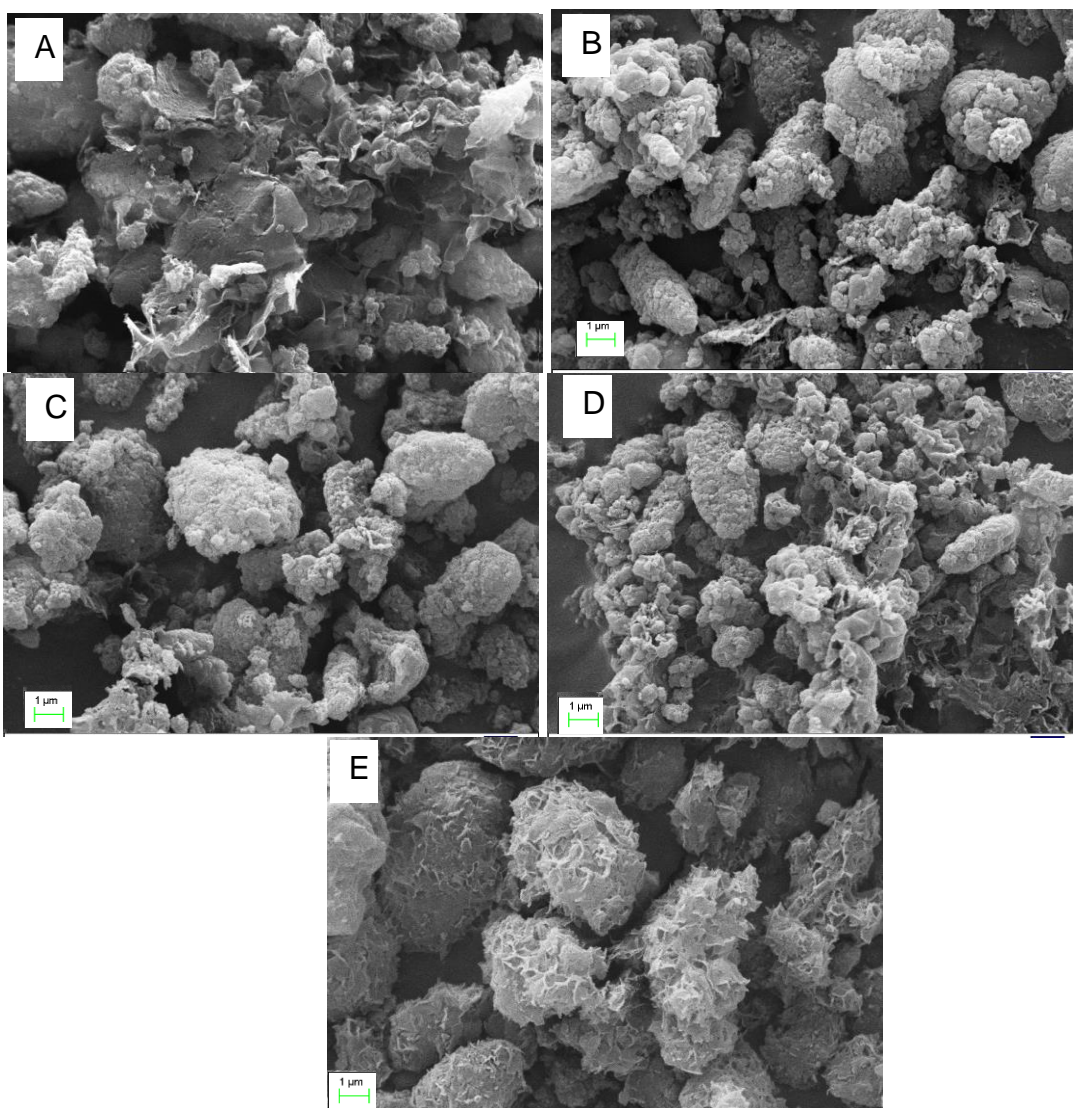


**Fig. 5.** Nitrogen adsorption isotherms of ACs obtained by a one-step activation method from various activation periods (AT = 900 °C; R = 3; v = 70  $\text{cm}^3/\text{min}$ )

The effect of the  $\text{N}_2$  flow rate on the yield, BET surface area, and pore volume is shown in Table 1 (entries 4, 11, and 12). The yield of ACs increased with increasing  $\text{N}_2$  flow rate. A possible reason for this is that the activating agents, including water vapor, CO, and  $\text{CO}_2$  formed under activation, were carried away rapidly by the high flow rate of inert gas (Foo and Hameed 2012). Therefore, the decrease of auxiliary activating agent with high  $\text{N}_2$  flow rate resulted in the carbon consumption decreasing and carbon yield increasing. The surface area increased from 1402.6 to 1816.3  $\text{m}^2/\text{g}$  and the pore volume increased from 0.81 to 1.26  $\text{cm}^3/\text{g}$ , respectively, as the  $\text{N}_2$  flow rate increased from 40 to 70  $\text{cm}^3/\text{min}$ . However, the surface area and pore volume decreased to 1528.6  $\text{m}^2/\text{g}$  and 0.89  $\text{cm}^3/\text{g}$ , respectively, when the  $\text{N}_2$  flow increased from 70 to 100  $\text{cm}^3/\text{min}$ . Figure 6 shows the  $\text{N}_2$  adsorption isotherms of the porous carbons prepared under various  $\text{N}_2$  flow rates at 900 °C for 2 h. As can be seen in Fig. 6, all isotherms exhibit type IV mesoporous development but they also reveal microporous structure. At 70  $\text{cm}^3/\text{min}$   $\text{N}_2$  flow rate, the mesoporosity was developed more than that of at 40 and 100  $\text{cm}^3/\text{min}$   $\text{N}_2$  flow rate.



**Fig. 6.** Nitrogen adsorption isotherms of ACs obtained by a one-step activation method from various  $N_2$  flow rates (AT =  $900^\circ C$ ;  $R = 3$ ;  $t = 2$  h)

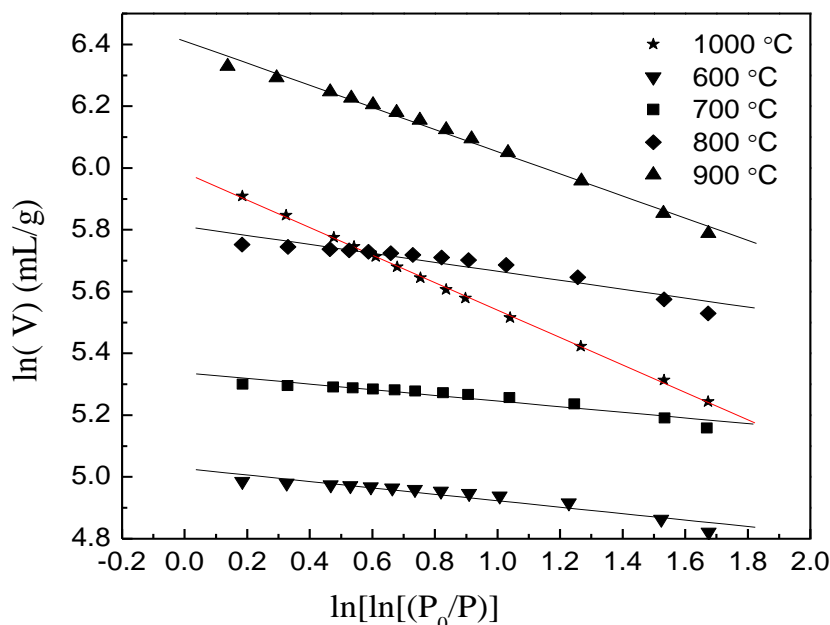


**Fig. 7.** SEM micrographs (20000x) of the ACs prepared by a one-step  $K_2CO_3$  activation method at A)  $600^\circ C$ , B)  $700^\circ C$ , C)  $800^\circ C$ , D)  $900^\circ C$ , and E)  $1000^\circ C$  ( $R = 3$ ;  $t = 2$  h;  $v = 70$   $cm^3/min$ )



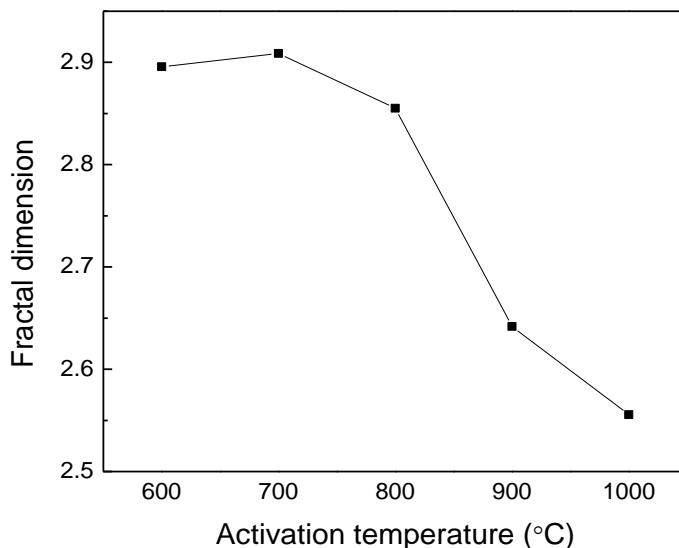
SEM images of the ACs activated at various temperatures are shown in Fig. 7(a-e). There were observable differences between the 600 and 1000 °C ACs. The surfaces of the ACs obtained at 600 °C were smooth and without any pores. Nevertheless, the external surfaces of these ACs activated at 700 to 1000 °C showed rich porosities that were too small to be fully observed and were very irregular. The ACs obtained at 1000 °C had a notably different morphology than the ACs activated at 700 to 900 °C because the mesopores and macropores of these ACs resulted from the evaporation of  $K_2CO_3$  during the 1000 °C carbonization, leaving behind spaces previously occupied by  $K_2CO_3$ .

Surface roughness is an important factor that influences the adsorption property of an adsorbent. The surface fractal dimension, based on the adsorption isotherm, is a measurement of surface roughness (Zhang *et al.* 2014b). The fractal FHH obtained from the isothermal data (relative pressure of 0 to 0.3) at various activated temperatures is plotted in Fig. 8. There was a good linear relationship between  $\ln(\ln(P/P_0))$  and  $\ln(V)$ . The results show that the fractal dimensions obtained from fractal FHH were reliable.



**Fig. 8.** Fractal FHH plots of ACs prepared from  $KL_d$  under various AT by  $K_2CO_3$  activation

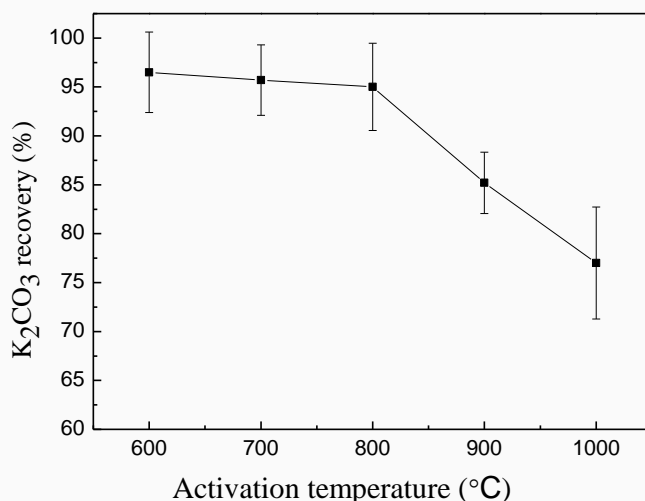
Figure 9 shows the influence of the activation temperature on the estimated fractal dimensions. The fractal dimensions of the ACs prepared by  $K_2CO_3$  decreased with an increase in the activation temperature.



**Fig. 9.** Influence of activation temperature on the fractal dimensions of ACs

Comparing the fractal dimension with the mesopore proportion in Table 1 at different activation temperatures, the ACs activated at 700 °C exhibited the greatest fractal dimension and the smallest proportion of mesopores. At 1000 °C, the fractal dimension of AC was the smallest; however, it exhibited the greatest mesopore proportion at 95.9%. These results show that the fractal dimensions were consistent with the proportion of mesopores present. In other words, the fractal dimension decreased with increasing proportion of mesopores. This result is consistent with a previous report by Gómez-Serrano *et al.* (2005).

The recovery ratio of  $K_2CO_3$  at various activation temperatures was investigated, and the results are shown in Fig. 10. The recovery ratio of  $K_2CO_3$  decreased slightly between 600 and 800 °C, and decreased notably above 800 °C (Fig. 10). The results indicated that  $K_2CO_3$  decomposed partially above 800 °C. By XRD characterization (not shown), the recovered  $K_2CO_3$  and pure  $K_2CO_3$  were found to have almost similar crystal structure, so the recovered activating agent can be reused in AC preparation.



**Fig. 10.** Recovery ratio of  $K_2CO_3$  at various activation temperatures

## CONCLUSIONS

1. The preparation and characterization of activated carbon from kraft lignin was investigated in this work. In comparison to the  $K_2CO_3$  to  $KL_d$  mass ratio, activation period, and  $N_2$  flow rate, the carbonization temperature played the most crucial role in the amount of final product, the surface area, and the pore volume.
2. The prepared ACs attained a surface area of  $1816.3 \text{ m}^2/\text{g}$ , a total pore volume of  $1.26 \text{ cm}^3/\text{g}$ , and a high contribution of mesopores at 95.9% when the  $K_2CO_3$  to  $KL_d$  mass ratio equaled 3, the activation temperature was  $900 \text{ }^\circ\text{C}$ , the activation period was 2 h, and the  $N_2$  flow rate was  $70 \text{ cm}^3/\text{min}$ .
3. The activating agent,  $K_2CO_3$ , can be partially recovered, and the washing water discharge can be minimized. From an economical and environmental standpoint, the use of a one-step chemical activation method is simple, efficient, low-cost, and environmentally friendly. This preparation method is suitable for large-scale, cleaner production of ACs with high mesoporous surface areas from KL by  $K_2CO_3$  activation.

## ACKNOWLEDGMENTS

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